

## **ELECTRONIC DEVICES AND METHODS FOR MAKING SAME USING NANOTUBE REGIONS TO ASSIST IN THERMAL HEAT-SINKING**

### **BACKGROUND**

The present invention relates to the electronics arts. It especially relates to flip-chip bonded light emitting diodes for lighting applications, and will be described with particular reference thereto. However, the invention will also find application in conjunction with die-bonding and cooling of other electronic devices.

Light emitting diodes are increasingly being employed in outdoor displays and signals, indoor illumination, and other applications that call for high levels of light output. To achieve improved light output, these devices are being driven with increasingly higher currents, resulting in thermally limited performance.

To improve heat removal, flip-chip mounted light emitting diodes have been developed. In the flip-chip arrangement, the active light emitting layers are grown on a transparent substrate, front-side contacts are fabricated on the light emitting layers, and the die is bonded front-side down to a lead frame, heat sink, or sub-mount so that light is emitted through the transparent substrate. The flip-chip arrangement places the heat generating active layers near the heat-sinking substrate or sub-mount, and also minimizes contact shadowing.

However, flip-chip bonding has certain disadvantages. Soldering is usually employed in the die-bonding. This involves substantial heating near the active layers which can degrade the device. If the die is bonded to a sub-mount, then two soldering processes are involved (a die-to-sub-mount soldering process and a sub-mount soldering process). The first soldering process is preferably

performed at higher temperature so that the first solder bonds remain stable during the second soldering process. Moreover, relatively thick solder bumps are often employed for reliability. These thick solder bumps can limit thermal transport out of the light emitting diode die.

- 5                   The present invention contemplates an improved apparatus and method that overcomes the above-mentioned limitations and others.

## BRIEF SUMMARY

- 10                   According to one aspect, a semiconductor device is disclosed, including a semiconductor device die. A heat-sinking support structure is provided, on which the semiconductor device die is disposed. Nanotube regions containing nanotubes are arranged on a surface of or in the heatsinking support structure. The nanotube regions are arranged to contribute to heat transfer from the semiconductor device die to the heat-sinking support structure.

- 15                   According to another aspect, a method of fabricating a semiconductor device is provided. A semiconductor device die is attached to a die support. Nanotube regions containing nanotubes are formed on or in the die support. The nanotube regions are configured to conduct heat away from the attached semiconductor device die.

- 20                   Numerous advantages and benefits of the present invention will become apparent to those of ordinary skill in the art upon reading and understanding the following detailed description.

## BRIEF DESCRIPTION OF THE DRAWINGS

- 25                   The invention may take form in various components and arrangements of components, and in various process operations and arrangements of process operations. The drawings are only for purposes of illustrating preferred embodiments and are not to be construed as limiting the invention. The device views are not drawn to scale.

FIGURE 1 shows a side view of a flip chip light emitting diode in position to be flip-chip die-bonded to a heat sinking support structure that includes die-bonding bumps including nanotube regions.

FIGURE 2 shows a suitable method for fabricating the heat sinking support structure of FIGURE 1.

FIGURE 3 shows nanotube bumps on the surface of a silicon wafer.

FIGURE 4 shows a top view of a heat sinking sub-mount with microchannels of the sub-mount shown in phantom.

FIGURE 5 shows a cross-sectional view of one of the microchannels of the heat sinking sub-mount of FIGURE 4.

FIGURE 6 shows a suitable method for fabricating the microchannels of the heat sinking sub-mount of FIGURES 4 and 5.

FIGURE 7 shows a side sectional view of an actively cooled sub-mount for a microelectronic device.

FIGURE 8 shows a top view of the actively cooled sub-mount of FIGURE 7, with the cooling system shown in phantom.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

With reference to FIGURE 1, a flip-chip light emitting diode die 10 is shown in position for die-bonding. The light emitting diode 10 includes a transparent substrate 12 and active layers 14, 16, 18 deposited on the substrate 12. In one suitable embodiment, the transparent substrate is sapphire or silicon carbide, and the active layers 14, 16, 18 are deposited by metal-organic chemical vapor deposition (also known by similar nomenclatures such as organometallic vapor phase epitaxy), molecular beam epitaxy, or another epitaxial film growth technique. The active layers 14, 16, 18 define a GaN-based p-on-n or n-on-p light emitting diode structure in which the layers 14, 18 are of opposite conductivity type and the interposed layer 16 defines an electron-hole pair recombination region at which electrons and holes from the outer layers 14, 18 recombine.

In some GaN-based light emitting diodes, the layer **16** is omitted and radiative recombination occurs principally around a junction of the layers **14**, **18**. Moreover, additional active layers can be included such as a window layer, a heavily doped contact layer, or the like. A growth buffer layer (for example of aluminum nitride) can be grown to improve the epitaxial growth. Moreover, other types of diodes besides GaN-based diodes can also be used, such as InAlGaP-based diodes, group III-arsenide-based diodes, and so forth.

The active layers **14**, **16**, **18** are processed, preferably lithographically, to define a mesa including the topmost layers **16**, **18**. Electrodes **20**, **22** are formed off and on the mesa to electrically contact the layers **14**, **18**, respectively. In a suitable embodiment, the electrodes include a thin adhesion and diffusion barrier layer **24** and a thicker die-bonding layer **26**, such as a nickel diffusion layer and a gold die-bonding layer. An adhesion layer (not shown) of titanium or another material can also be included. Although layer materials **24**, **26** are shown for both electrodes **20**, **22**, different materials and/or more or fewer layers can be provided for the electrodes **20**, **22** to produce electrode stability and electrical contact properties suited for each of the layers **14**, **18**, respectively.

The flip chip light emitting diode die **10** is die bonded to a heat sinking support assembly **30**, which can be a sub-mount, printed circuit board, or the like. The support assembly **30** includes a support **32** on which is disposed conductive layers **34**, **36**. The conductive layers **34**, **36** optionally are part of printed circuitry, interconnect metallizations, wire bonding pads, or the like. The conductive layers **34**, **36** are connected to external circuitry (not shown) for energizing the light emitting diode die **10** to emit light.

Disposed on each of the conductive layers **34**, **36** is a bonding bump **40**, **42**, respectively. The bonding bumps **40**, **42** are arranged to conform with an arrangement of the electrodes **20**, **22** of the light emitting diode **10**. The bonding bumps **40**, **42** include a catalyst layer **50** of a metal, a metal alloy, or another material suitable for nucleating growth of nanotubes. A nanotube region **52** containing nanotubes **54** is grown on the catalyst layer **50**. A few exemplary

nanotubes **54** are shown diagrammatically in FIGURE 1; however, the nanotube packing density is preferably much higher than that shown, and in one preferred embodiment the nanotube density is high enough so that neighboring nanotubes are in occasional contact.

5                   Single-walled or multiple-walled carbon or boron compound nanotubes are suitably grown on the catalyst layer **50** by chemical vapor deposition or another suitable deposition technique. In chemical vapor deposition, the catalyst layer **50** is exposed to a hydrocarbon ambient at an elevated temperature. As is known in the art, nanotubes spontaneously form under such  
10 conditions for certain ambient temperatures and hydrocarbon ambient compositions and pressures. Nanotube growth can be controlled by selecting the temperature and ambient composition and properties, and by controlling the growth time. Preferably, the growth conditions are selected to produce a high density of generally parallel nanotubes that grow in a direction generally extending  
15 away from and normal to, the catalyst layer **50**, as shown diagrammatically in FIGURE 1.

                  The nanotube regions **52** define nanotube bonding bumps for die-bonding the flip-chip light emitting diode **10** to the support assembly **30**. The nanotube bonding bumps are preferably coated with die-bonding metal layer  
20 stacks **60**. In one suitable embodiment, each bonding stack **60** includes a titanium adhesion layer **62**, nickel diffusion barrier layer **64**, and a gold die-bonding layer **66**. The light emitting diode die **10** is shown in position for die-bonding, but before bonding. In a preferred embodiment, the die bonding is performed by thermosonic gold-to-gold bonding in which the support assembly **30** is heated to about 150 °C  
25 with the bonding bump gold layers **66** contacting the corresponding electrode gold layers **26** of the light emitting diode **10**. Upon application of ultrasonic energy, the gold layers **26**, **66** bond, forming a die-attachment that is thereafter thermally stable up to about 600 °C. Although thermosonic bonding is preferred, soldering or other die-bonding techniques are optionally employed in the die-bonding.

Once bonded, the nanotube regions **52** provide a highly thermally conductive path between the light emitting diode **10** and the substrate **30**. While typical solders have thermal conductivities of about 25-60 W/mK and bump heights of greater than 25 microns for reliability, by contrast carbon nanotubes exhibit thermal conductivities typically over 1000 W/mK over a typical operating temperature range for a light emitting diode or other electronic device of about 0-150 °C. Moreover, nanotubes are generally electrically conductive to provide an electrical path for energizing the light emitting diode **10**.

Nanotubes have anisotropic thermal properties with maximum thermal conductivity along the axis of the nanotube, and so the preferred generally aligned nanotube orientation shown in FIGURE 1 provides maximum thermal conduction from the light emitting diode **10** to the substrate **30**. Advantageously, nanotubes **54** extending generally away from the catalyst layer **50** typically grow spontaneously under suitable deposition conditions. Some bending, intertwining, or other deviation of some or most nanotubes away from the generally aligned and straight nanotube orientation shown in FIGURE 1 is contemplated; however, this does not obviate the substantial advantageous thermal and electrical properties of the nanotube regions **52**. For example, predominantly helical nanotubes, also called nanosprings, are formed under certain deposition conditions. Moreover, the nanotubes **54** can be substantially filled. Filled nanotubes are also known in the art as nanorods. The nanotubes **54** of the bonding bump nanotube regions **52** are preferably columnar nanorods having relatively large cross-sectional areas (corresponding to diameters of about a hundred nanometers or more) to provide for substantial thermal conduction.

Those skilled in the art can readily modify the above-described exemplary flip-chip light emitting diode die **10** and/or substrate **30** to include additional or fewer active layers, different substrate and/or active layer materials, and the like. The light emitting diode die can also be configured with back-side contacts, rather than front-side contacts, using known fabrication techniques. Moreover, other types of semiconductor devices can be similarly bonded. For

example, a transistor could be die bonded to nanotubes-based bonding bumps. It will further be appreciated that more than two electrodes can be die bonded. For example, a microprocessor chip including a large number of electrodes can be die-bonded using a plurality of corresponding nanotubes-based bonding bumps.

5           It is contemplated to optionally employ both nanotubes-based bumps and conventional copper or other metallic bonding bumps in a bonding pad configuration. In such an arrangement, the nanotubes-based bonding bumps are preferably arranged in high heat flux regions, while conventional copper bonding bumps can be employed in cooler device regions. The particular arrangement or  
10   distribution of bonding bumps is selected based on application and thermal managements considerations. Moreover, rather than employing local nanotubes-based bonding bumps, the entire sub-mount surface can be coated with nanotubes to provide for both heat extraction and lateral heat spreading. In such a uniform arrangement, electrical conductivity considerations should be considered.  
15   The uniform nanotubes layer may be patterned to provide electrical isolation between bonding pads or devices. Alternatively the bumps may be fabricated on the active device, i.e. LED, transistor, rather than on the submount or board. The same metal termination stacks would apply.

          With continuing reference to FIGURE 1 and with further reference to  
20   FIGURE 2, a suitable process 70 for fabricating the bonding bumps 40, 42 is described. The process 70 starts with providing a mounting or support assembly 72 that includes conductive layers such as the conductive layers 34, 36 shown in FIGURE 1. The conductive layers can be printed circuitry, interconnect metallizations, wire bonding pads, or the like. The catalyst layer material is applied  
25   over the mount or support assembly in a deposition 74. The deposited layer is patterned 76, preferably lithographically, to remove the deposited layer except in the region of the bonding pads, leaving the lithographically defined catalyst layer 50 shown in FIGURE 1.

          After the patterning 76, the nanotube regions 52 are grown 80 by  
30   chemical vapor deposition using suitable ambient chemistry and pressure,

process temperature, and like growth parameters. For boron alloy nanotubes, a boron-containing ambient is used in the chemical vapor deposition. The nanotube regions **52** are metallized in a lift-off metallization process **82**, **84**, **90**, **92**. In the liftoff process, resist is applied **82**, followed by lithographic patterning **84** to expose the nanotube regions **52**. A suitable sequence of metal layers is deposited **90**, and the resist is removed or stripped **92**. During the resist stripping **92**, the overlying metal layers are lifted off except in the nanotube regions **52**, where the metal remains as the die-bonding metal layer stacks **60** of the support assembly **30** shown in FIGURE 1.

Rather than using the lift-off process **82**, **84**, **90**, **92**, in another suitable lithographic processing sequence (not shown) the metal is first deposited, followed by resist application and patterning to protect the deposited metal on the nanotube bumps. The exposed metal is then etched away leaving only metal on the nanotube bumps. Finally, the resist on the nanotube bumps is stripped.

With reference to FIGURE 3, an array of exemplary carbon nanotube bumps **94** grown on a silicon wafer **96** is shown. Each nanotube bump **94** includes a high density of generally aligned nanotubes. The nanotubes were grown by metal-organic chemical vapor deposition (MOCVD, also known as organometallic vapor phase epitaxy and similar nomenclatures). However, other types of chemical vapor deposition can also be employed, as well as other deposition techniques such as thermal evaporation, laser ablation, sputtering, and the like. Moreover, nanotubes of boron nitride, silicon, copper, or another suitable material can be employed instead of carbon nanotubes.

In a suitable nanotubes bumps growth process, the silicon substrate is cleaned in deionized water and then annealed at 700°C in air for 5 minutes to develop a substantially uniform oxide layer, and to remove any adhering organic materials. The cleaned wafer is lithographically patterned using a metal mask and UV lamp operating at about 365nm. The photoresist is developed and post-cured before deposition of the nanotubes bumps. Any wavelength is acceptable as long as it can expose the photoresist.



Nanotubes deposition is performed in a quartz reactor tube, which in one suitable embodiment includes a 2.5 cm diameter quartz tube with two temperature zones: a short zone at the inlet to the reactor, and a long zone where the reaction and deposition takes place. In a typical deposition, the first zone is set at about 175°C and contains the gas inlet and a capillary steel tube with a crimped end that is used as a spray head. The second zone is in a clamshell furnace set approximately between 750°C and 950°C. Higher temperatures tend to produce straighter nanotubes but may reduce coverage density. The isothermal zone of quartz reactor tube in one embodiment is about 30 cm long, with about a 20°C temperature variance across the length.

After the substrates are loaded into the reactor tube, the system is purged with dry argon gas at about 1 standard liter per minute (SLPM), after which the gas composition is changed to about 10% hydrogen in argon at the same flow rate. The two oven zones are heated to their target temperatures. After an approximately 15 minute pause for equilibration, a hydrocarbon ambient including a carbon source and a catalyst are introduced.

The hydrocarbon ambient is suitably produced by pyrolyzing a mixture of a volatile metal species along with a carbon source. In one suitable deposition arrangement, the carbon source is an aromatic hydrocarbon such as xylene, and the catalyzing volatile metal species is ferrocene (dicyclopentadienyliron, CAS # 102-54-5). The catalyst concentration in the xylene is about 12 milligrams/ml. The solution of ferrocene in xylene is introduced via a syringe pump at a rate of about 45 microliters/min. After about 5 ml of solution is introduced, the system is held at temperature for 10 minutes to insure removal of all volatiles, and then cooled to below 200°C before switching from the 10% hydrogen to pure argon. When the reactor reaches ambient temperature with the help of a cooling fan, the tube is opened and the coated substrates removed.

The exemplary conditions above typically produce a mixture of aligned multi-wall and single wall carbon nanotubes with an average length of

about 120 to 150 microns. Some multiwall tubes have diameters of about 25 nm. The tubes typically contain residual iron from the catalyst.

It will be appreciated that the described growth process is exemplary only. Those skilled in the art can readily adapt the described growth process, or  
5 apply another growth process, to generate suitable nanotube regions for specific applications using available deposition facilities. For example, a physical vapor deposition method such as glancing angle deposition (GLAD) can be employed to produce nanotubes predominantly in the form of nanocolumns, nanorods or elongated nanosprings. Other approaches to aligned patterned nanotubes include  
10 nano-contact printing and other methods of applying nanotube growth catalysts on a substrate.

An exemplary suitable light emitting device embodiment has been described with reference to FIGURES 1-3, in which nanotube regions **52** are configured as components of die-bonding bumps **40**, **42** to assist in thermal heat-sinking by providing a highly thermally conductive path from the light emitting  
15 diode **10** to the heat sinking support assembly **30**. The heat sinking support assembly **30** may itself be a substantial thermal reservoir that dissipates heat, or it may be a heat sinking sub-mount that is thermally conductive and in thermal communication with a heat reservoir that dissipates heat.

20 In the case of a heat sinking sub-mount arrangement, heat dissipation is improved by ensuring that the sub-mount distributes heat laterally across the sub-mount to quickly remove the heat from the attached electronic device, and to assist in rapid dissipation of heat to the underlying heat reservoir. In the case of high-power light emitting diodes, a heat sinking sub-mount is typically  
25 fabricated from a silicon or silicon carbide wafer, which has relatively high thermal conductivity and which can be made substantially electrically insulating.

To improve lateral heat transfer of the heat-sinking sub-mount, a lateral heat-spreading film or structure **98** is optionally formed on the sub-mount. In one preferred embodiment, the structure **98** is diamond film grown by chemical  
30 vapor deposition, poly-crystalline deposition, or the like. In another contemplated

embodiment, the structure **98** comprises nanotubes that substantially cover the sub-mount surface. Boron nitride nanotubes that are thermally conductive but substantially electrically insulating are beneficially employed for this purpose. The thermally conductive heat-spreading film **98** is especially beneficial for mounting  
5 more than one light emitting diode chip on a single sub-mount, for mounting a small light emitting diode chip on a substantially larger sub-mount, for other arrangements in which a lateral area of the sub-mount is large compared with a lateral area of the one or more mounted light emitting diodes.

With reference to FIGURES **4** and **5**, another embodiment of the  
10 invention is described, in which nanotube regions are configured to provide heat spreading in a heat-sinking sub-mount **100**. This embodiment provides another mechanism for improved lateral heat transfer that uses nanotubes. Those skilled in the art will appreciate that good lateral heat transfer in electronics support elements is of general benefit to many areas of microelectronics and photonics,  
15 and its benefits are not limited to light emitting diodes. Efficient lateral heat transfer in the mount facilitates cooling of electronic or photonic chips in both flip-chip and conventional bonding arrangements. For certain such applications, boron nitride nanotubes are advantageously used to combine high thermal conductivity with low electrical conductivity. Thus, boron nitride-based nanotubes are  
20 particularly suitable for providing electrically insulative regions of high thermal conductivity.

The sub-mount **100** includes a bottom silicon sub-mount wafer **102** and a top silicon sub-mount wafer **104** that are anodically bonded via an oxide layer **106** disposed therebetween. Rather than anodic bonding, an adhesive or  
25 other type of bonding can be employed. Patterned conductive layers **110** are disposed on an exposed surface **112** of the top sub-mount wafer **104**. Die bonding pads **114** are arranged on the conductive layers **110**. The conductive layers **110** supply electrical power to a semiconductor device **116** such as a light emitting diode, microprocessor chip, or transistor, that is die-bonded to the bonding pads

**114.** The die-bonding pads **114** optionally include nanotube bumps such as the nanotube regions **52** of FIGURE 1.

A plurality of thermally conductive microchannels **120** are shown in phantom in FIGURE 4, and one of the microchannels **120** is shown in cross-section in FIGURE 5. As shown in top view (see FIGURE 4), the microchannels **120** extend laterally away from the die-bonding region in various lateral directions. (The die-bonding region is a region around the bonding pads **114** where heat from the attached semiconductor device **116** is injected into the heat sinking sub-mount **100**). As shown in cross-sectional view (see FIGURE 5), each thermally conductive microchannel **120** is defined by a groove **122** formed in the bottom sub-mount wafer **102** that is capped by the top sub-mount wafer **104** (or more specifically, capped by the oxide layer **106**). The grooves **122** preferably have widths of about a few microns to a few tens of microns. Although a plurality of unconnected microchannels **120** are shown in FIGURE 4, the microchannels can instead interconnect at the die-bonding region by intersection of the grooves **122**.

A catalyst coating **124** is applied on surfaces of the microchannel **120**. A thermal conductivity-enhancing nanotube region containing nanotubes **126** grown on the catalyst coating **124** is disposed inside the microchannel **120**. A few exemplary nanotubes **126** are shown diagrammatically extending from the bottom of the groove **122** in FIGURE 5; however, the nanotube density is preferably much higher than that shown in FIGURE 5, and nanotubes preferably extend into the microchannel **120** from various sides of the groove **122** in addition to the bottom of the groove **122**.

The microchannels **120** assist in lateral thermal conduction away from the die-bonding region. In the illustrated embodiment of FIGURE 5, the microchannels **120** act as heat pipes, in which a fluid such as water conducts heat away from the die-bonding region by an evaporation/condensation cycle. Near the die-bonding region, the fluid is evaporated due to heat generated by the semiconductor device **116**, to produce fluid vapor **130** (represented by shading in FIGURE 5). The fluid vapor **130** diffuses away from the die-bonding region along

the length of the microchannel **120**. At an end of the microchannel **120** that is distal from the die-bonding region, the fluid vapor **130** condenses to form fluid droplets **132**. Heat is conducted by the diffusing vapor and released by the condensation process. The condensed fluid accumulates and flows back toward the die-bonding region, where it re-evaporates to complete the evaporation/condensation cycle.

Rather than or in addition to heat pipe evaporation/condensation heat transfer, the microchannels can operate by thermal conduction through a substantially continuous liquid or gas disposed in the microchannels. For example, the microchannels can be air-filled or water-filled.

Thermal transfer through the microchannels **120** is assisted by the nanotubes **126** in several ways. The nanotubes **126** provide improved thermal coupling to surfaces of the grooves **122** to assist in heat transfer from the working fluid to bulk material of the heat sinking sub-mount **100**. Nanotubes **126** also assist in fluid mixing. Moreover, the nanotubes **126** enhance capillary action in the microchannels which assists in migration of condensed fluid back to the die-bonding region. Still furthermore, nanotubes **126** create turbulence at the surfaces of the grooves **122**. This turbulence inhibits formation of stagnant fluid layers at surfaces of the grooves **122**. Nanostructures create flow disturbances which can be considered as local turbulences, although the bulk flow might be in the laminar flow regime. It will be appreciated that the spontaneously formed arrangement of the nanotubes, which extend generally inward from the groove surfaces, that is, aligned generally perpendicular to an axis of the groove, is particularly advantageous for creating turbulence and for transporting heat from interior regions of the microchannels **120** to the groove surfaces. However, substantial benefits will also be obtained from less ideal nanotube configurations that may be produced by certain growth conditions.

With continuing reference to FIGURES **4** and **5**, and with further reference to FIGURE **6**, a suitable process **140** for fabricating the sub-mount **100** is described. Processing of the bottom sub-mount wafer starts with groove

formation **142**, which suitably includes lithographically patterned etching in which an applied and patterned resist defines lateral dimensions of the grooves **122**. Anisotropic etching is optionally used to define a selected groove shape or faceted or otherwise configured groove surfaces.

5                   In deposition **144**, the catalyst coating is applied to the groove surfaces. The catalyst coating is a metal or other thin film that is effective for nucleating growth of nanotubes. In a suitable embodiment, the catalyst coating is applied before the patterned resist used in groove formation **142** is stripped off, so that the resist provides masking for the catalyst deposition **144** as well. The  
10                   nanotubes **126** are grown by chemical vapor deposition **146**. For a suitable ambient chemistry, pressure, temperature, and other growth parameters, a region of nanotubes with selected properties grows on catalyst-coated surfaces of the grooves **122**. Other approaches to aligned patterned nanotubes can include glancing angle deposition (GLAD), nano-contact printing and other methods of  
15                   applying nanotube growth catalysts on a substrate.

                  In separate processing, the oxide layer **106** is formed by oxidation **150** on the top sub-mount wafer, for example by thermal oxidation of the top sub-mount wafer in an oxygen-rich ambient. The oxidized surface of the top sub-mount wafer is joined **152** to the surface of the bottom sub-mount wafer on which  
20                   the grooves **122** are etched. In a preferred joining process, the two wafers are anodically bonded together by a combination of mechanical pressure and electrical biasing. However, other types of bonding can be employed. For certain bonding processes, such as bonding by the use of an adhesive, the oxidation process **150** is suitably omitted.

25                   Optionally, the working fluid **130**, **132** is introduced into the grooves **122** prior to or during the wafer bonding process **152**. If the working fluid is intended to be air, the working air fluid is naturally trapped in the grooves **122** during the joining process **152**. For water or another liquid working fluid, the fluid can be introduced by spinning the fluid onto the bottom sub-mount wafer **102'**, by  
30                   application with a squeegee, or the like prior to the joining process **152**. For a

gaseous working fluid other than air, the wafer joining process **152** can be performed in a suitable ambient so that the desired working gas is trapped in the sealed grooves **122**. The resulting joined wafer assembly preferably undergoes further processing **156** to deposit and pattern the conductive layers **100**, form the bonding bumps **114**, dice the joined wafer assembly to produce individual sub-mounts, and so forth.

In the apparatus **100** and fabrication process **140** of FIGURES 4-6, grooves are formed only in the bottom sub-mount wafer **102**. However, the grooves can instead be formed in the top sub-mount wafer. Moreover, matched grooves can be formed in both the bottom and top sub-mount wafers and combined during wafer joining to define the microchannels. Furthermore, the microchannels can have lateral configurations other than the illustrated radiating linear configuration. For example, a rectangular microchannel grid or an array of concentric circular microchannels of increasing diameter can be used to spread and distribute heat laterally across the sub-mount. Microchannel regions can also extend other than laterally through the sub-mount. For example, microchannels can be disposed in vias oriented generally perpendicularly to the sub-mount, to assist in heat transfer through the sub-mount.

The microchannels **120** can have substantially any cross-sectional shape, such as a circular, rectangular, square, triangular, octagonal, pentagonal, or other cross-sectional shape. A hydraulic diameter  $D_h$  of the channel wall is defined in terms of the cross-sectional area  $A_{cross}$  and the wetted perimeter  $P_{wet}$  according to  $D_h = (4 A_{cross})/P_{wet}$ . The hydraulic diameter  $D_h$  scales with the ratio of cross-sectional area  $A_{cross}$  to wetted perimeter  $P_{wet}$ , and so cross-sectional shapes with large  $A_{cross}/P_{wet}$  ratios are preferred for good thermal conduction.

With reference to FIGURES 7 and 8, a sub-mount employing actively cooled microchannels is described. A heat-generating device **200** is bonded to a sub-mount **202** that is actively cooled. The heat-generating device **200** can be a high-power light emitting diode, a microprocessor chip, or the like. More generally, the device **200** can be any type of device that generates

substantial heat and is advantageously actively cooled. The sub-mount **202** include a top portion **204** and a bottom portion **206** that are bonded together. In one preferred embodiment, the top portion **204** is a silicon wafer while the bottom portion **206** is made of flexiglass. However, other materials can be used.

5           The bonding surface silicon top portion **204** is machined or lithographically processed to define entrance and exit fluid reservoirs **210**, **212** and a plurality of microchannels **214** that connect the fluid reservoirs **210**, **212**. The bottom portion **206** includes larger entrance and exit fluid reservoirs **220**, **222** that join the entrance and exit fluid reservoirs **210**, **212**, respectively, of the silicon  
10 top portion **204**. A fluid inlet **226** is formed into the bottom portion **206** and is in fluid communication with the entrance fluid reservoir **220**. A fluid outlet **228** is formed into the bottom portion **206** and is in fluid communication with the exit fluid reservoir **222**. These features can be formed by machining, lithographic processing, or the like. The bottom and top portions **204**, **206** of the sub-mount  
15 **202** are secured together by an adhesive, mechanical clamping, or other suitable attachment mechanism.

A recirculating cooling system **230** is connected between the fluid inlet **226** and the fluid outlet **228**. The recirculating cooling system **230** includes a pump **232**, which can be an axial, centrifugal, or other type of pump, and a heat  
20 exchanger **234**. Arrows in FIGURE 7 indicate flow direction of a working fluid that flows through the recirculating cooling system **230** and the sub-mount **202**. The working fluid can be water, a dielectric fluid, oil, or the like. The heat exchanger **234** can be a thermoelectric cooling device, a passive radiator, or the like. Moreover, an open-loop cooling system can be employed instead of a closed-loop  
25 cooling system. The components **232**, **234** of the cooling system **230** are shown as separate from the sub-mount **202** and connected to the fluid inlet **226** and fluid outlet **228** of the sub-mount **202** by fluid pathways; however, it is also contemplated to have some or all components of the cooling system attached to and supported by the sub-mount.



To promote heat transfer from the sub-mount **202** to the circulating fluid, the microchannels **214** include nanotubes **240** (shown diagrammatically in FIGURE 7) extending inwardly in substantially aligned fashion from the walls of the microchannels **214**. The nanotubes **240** are suitably deposited after the  
5 microchannels **214** are formed into the silicon top portion **204**, but before the silicon top portion **204** is secured to the bottom portion **206**. Since heat extraction from the sub-mount **202** to the working fluid is a function of the surface area of the nanotubes **240** and the fluid turbulence generated by the nanotubes **240**, helical or otherwise-bent nanotubes, such as nanosprings **240** that are diagrammatically  
10 represented in FIGURE 7, are preferred. However, straight hollow nanotubes, filled nanorods, or otherwise-shaped nanotubes can also be employed.

The density and average length of the nanotubes **240** is selected to maximize thermal transfer while permitting good fluid flow. A ratio of nanotube height to hydraulic diameter  $D_h$  of close to unity (corresponding to the nanotubes  
15 substantially fully filling the cross-sectional area of the microchannels **214**) provides good heat transfer but is likely to substantially impede fluid flow. Lower nanotube-to-hydraulic diameter height ratios enhance fluid flow at the expense of reduced heat transfer from the sub-mount **202** to the working fluid. Similarly, the density of nanotubes **240** on the walls of the microchannels **214** can be selected  
20 in a range of close to 0% (low nanotubes density) to close to 100% (high nanotubes density). Higher nanotubes densities promote heat transfer, while lower nanotubes densities enhance fluid flow.

For cooling high power light emitting diodes using 0.2 mm diameter microchannels, computer modeling suggests that about ten microchannels  
25 underneath the light emitting diode along with one microchannel on either side of the device (twelve channels total, as illustrated in FIGURE 8) is adequate for cooling the light emitting diode. Additional microchannels beyond twelve can be used, however, and it is also contemplated to replace the microchannels **214** with a planar cooling plate, that is, a thin planar etched region of the top sub-mount,

inside of which nanotubes are formed, that provides fluid flow and heat extraction in the area of the sub-mount lying beneath the heat-generating device.

The invention has been described with reference to the preferred embodiments. Obviously, modifications and alterations will occur to others upon  
5 reading and understanding the preceding detailed description. It is intended that the invention be construed as including all such modifications and alterations insofar as they come within the scope of the appended claims or the equivalents thereof.